

APPROXIMATING SURFACE MATRIX BAND FOR DENTIST TO USE FOR PATIENTS

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Abstract

Background

Our objective is to create a dual matrix-band which can provide a tooth contour for the filling composite applied to adjacent teeth undergoing restoration. The following is an account of our design, manufacturing, and testing plans formed to successfully produce a dual matrix band which may alleviate the tedium of installing individual matrix bands on adjacent teeth undergoing restoration.

Methods

To achieve dimensional precision, the team outsourced fabrication to Big Blue Saw Manufacturing. Due to a delay in shipment, mechanical testing was conducted on feeler gauges of the same material and similar thickness to model and predict the device's mechanical performance. Functional testing, however, was executed using the prototype to assess the viability of the product post manufacturing.

Results

SolidWorks simulations showed that a band with half the thickness of a regular Tofflemire band was strong enough to withhold average forces during a restoration. Mechanical testing revealed

no useful results as each band slipped out of the MTS machine during testing so results were discarded. Functionality testing was performed, and according to the questionnaire metric by which the device's physical performance was measured, the prototype received a failing score of 47/65. To be deemed an optimal device, the prototype should have scored at least 62/65 or above (top 5% of scores).

Conclusions

Functionality testing results suggest that further design alterations must be considered to improve the ease of use and success of the prototype. We would like to perform functionality testing at least a total of 5 times with different people to get an average score (as functionality is highly subjective). Upon redoing mechanical testing with the prototype--with the bands fully reinforced in the MTS machine-- as well as obtaining an average functionality score, then we may conclude whether this design is a viable solution or not.

Practical Implications

The viability of our design will provide dentists with another matrix band alternative which gives support to adjacent teeth undergoing repair, maintains a tight and flossable tooth contact, and reduces the procedure time

Key Words

Matrix Band ▪ Class II Restoration ▪ Cavity

Tooth decay is a very common and painful experience approximately 91% of adults 20 - 64 years of age suffered from in 2011-2012 [1]. In addition, dental caries, also known as cavities, are the most prevalent disease that affects both children and adults [2]. The rise in dental caries has been labeled as a “pandemic” of sorts to highlight the prevalence, severity, and sometimes life-threatening, impact of tooth decay [3]. There are a plethora of methods to repair dental carries--which also depend on the severity of the cavity--however, the most common method is dental restoration (or dental fillings) [4]. As dental fillings serve as one of the primary means to

repairing tooth decay, it is a procedure dentists dedicate several hours a day to perform. Therefore, it is critical that dentists can efficiently and effectively perform restorative procedures in order to tend to as many patients possible. The process of filling a cavity varies in duration and complexity depending on the severity and classification of the cavity, and class II cavities--cavities on the interproximal surfaces of the premolars and molars [5]-- prove to be very challenging to restore because of the need to maintain a tight contact and maintain the tooth contour[6]. Matrix bands are meant to assist dentists by providing a contours to follow when filling the decayed tooth, and when used with tooth wedges (designed to increase the tooth contact gap), they are fairly accurate in recreating a tight contact, however, matrix bands fail when dentists must perform dental filling procedures on two adjacent class II cavities. Because matrix bands have a thickness which exceeds the contact gap between the teeth, and the tooth wedge is not capable of increasing the tooth contact gap beyond the thickness of a single matrix band, dentists have no option but to extend the total procedural time and perform restoration on one tooth at a time.

Our client is well versed with the Tofflemire matrix band, which is a popular matrix band used by dentists. The Tofflemire matrix band comes in a variety of thicknesses (ranging from 0.0015 - 0.002 in [7] which allows space for adjustment from patient to patient, it is very simple for dentists to use in junction with a retainer (used to tighten and maintain the desired band shape) and tooth wedges or rings(used to increase the contact gap between teeth), and it is very inexpensive (approximately \$10.00 for 100 bands [8]). The Tofflemire band is also very effective in maintaining a tight tooth contact and providing adequate structural support when forming the filling materials, however, it is not possible to place two bands adjacent to each other when restoring two interproximal cavities. Our client has found this caveat to make some filling procedures unnecessarily tedious and repetitive.

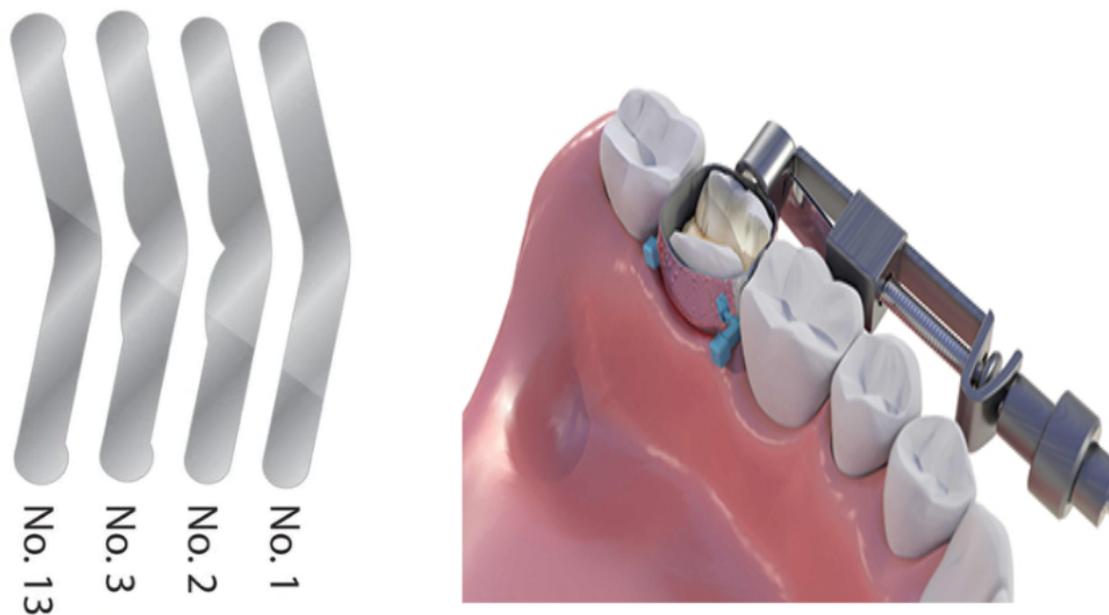


Figure 1: Image of a universal Tofflemire matrix band unformed (left) and formed around the tooth in the standard set up. The tooth wedge (used to increase the contact gap) and retainer (used to maintain the band shape) are also depicted in the right image. [10][11]

The Sectional matrix band is another widely used alternative. The Sectional matrix functions to give form to the restoration material and provide a tight contact, as the Tofflemire, however instead of encircling the entire tooth, the Sectional matrix only supports the section of the tooth that is undergoing repair. It is more space efficient than the tofflemire as it does not require a retainer to maintain its form around the tooth (the Sectional matrix requires a more compact tooth ring to keep it sturdy instead). Similar to the Tofflemire matrix band, the Sectional matrix band varies in sizes to better accommodate the patients tooth morphology, it is also exceptional in maintaining tight tooth contact, although it is more expensive in contrast to the Tofflemire band (approximately upwards of \$60.00 for 100 pieces[12]).

Matrix bands are a commonly used dental tool which assist dentists by providing a wall to maintain a tooth's structure and shape during restorative procedures, such as cavity fillings[13]. During typical filling procedures--particularly filling cavities on interproximal surfaces--dentists must fill one tooth at a time since matrix bands cannot be placed adjacent to one another, as the thickness of two bands exceeds the aperture diameter between the teeth. The resulting process of placing matrix bands for both teeth is cumbersome and time inefficient. Our

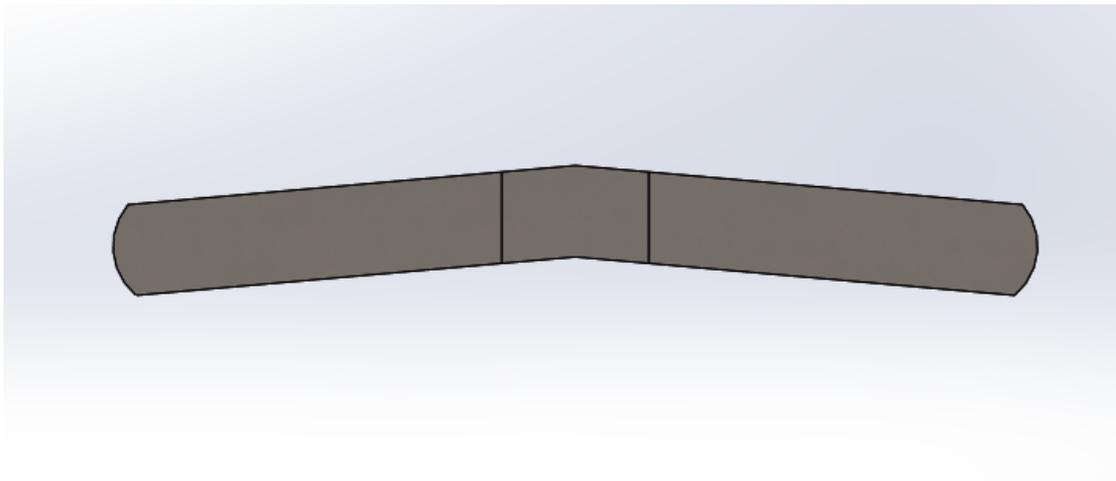
matrix band design alleviates the need to repeatedly place bands by employing a dual band system which is thin enough to securely and comfortably fit in between the affected teeth and able to simultaneously fit the appropriate convex/concave contour of each tooth. Upon testing, the finalized product should also maintain the tensile strength, malleability, and space efficiency of current matrix bands. Our Client, Dr. Donald Tipple, is a dentist at Nakoma Dental, has requested that we create a dual matrix-band which can provide a contour and support for the filling materials for adjacent teeth undergoing restoration. The client's primary request was that the device be constructed from non-toxic materials, and the device mechanism should encourage a tight but flossable contact between the affected teeth. In addition, the device should be equally or less costly to manufacture than current matrix bands, and the device should not be obstructive or clash with other tools to be used (rotary instruments, mirrors, forceps, suction etc.). Lastly, the band material should be thin and have high tensile strength.

Methods

The "Doug" is essentially a modified version of the current device that our client uses, therefore, the traditional material of choice (most likely the 316L type stainless steel based on its biocompatibility and corrosion resistance [14]) will be used in the fabrication of our prototype. We suspect the palodont tooth wedge (or any tooth wedge) would be compatible to use with our dual matrix band system. For testing purposes, two retainers will be used to tighten the matrix bands and hold their position, however, future work will warrant an updated retainer which can accommodate two bands.

Fabrication planning began with determining the required thickness of the double-sided band through our preliminary research, and the matrix band thickness was determined to be somewhere in the range of .0015 - .002 inches. We presumed that making each matrix band--the portion of the band that is placed between the teeth-- half this thickness (0.00075 - 0.001 in) will ensure that the thickness when the two bands are adjacent to one another does not exceed the natural tooth contact gap. To achieve this idea, we intended to fabricate each band by taking a sheet of 316L type stainless steel (of 0.002 in thickness and about 3 in in length) and thinning a 1x1in square at the center of the band to 0.001 inches in thickness. To assess the viability of the final design before fabrication, mechanical testing on SolidWorks was completed. This

quantitative test gave preliminary data on how the prototype would compare to bands used in the clinic now in terms of the stress and strains put on them. Figure 2 shows the SolidWorks model of the matrix band used today, which was the control for the experiment. Figure 2 shows the SolidWorks model of our final design. This design consisted of the same material and same overall shape as the control, but with slightly different dimensions. AISI Type 316L stainless steel was used as it is often a material used for medical and chemical devices, but not as expensive as the medical grade type 316L stainless steel. Since any 316L stainless steel is biocompatible, it might not be necessary to get the stainless steel used for implants, or the medical grade [14]. For this experiment, a 62% incline was added to the middle 1 cm of the band. This allowed for a decrease in thickness towards the middle while keeping the integrity of the rest of the band. The exact middle was half the thickness of the band, while everything farther than 0.5 cm from the middle remained the full thickness. In this experiment, a band of 0.0038 cm thickness was used, which is the smaller of the two bands used in practice. To attain the precision we desired for the center thickness of the matrix band, we entertained the idea of outsourcing fabrication, as we lacked the machining skills and the 3D printer quality to do it ourselves. We were able to partner with Big Blue Saw manufacturing company, and they agreed to waterjet cut 20 prototypes for us. However, due to a delay in payment, we were unable to receive our devices until after our final presentation.



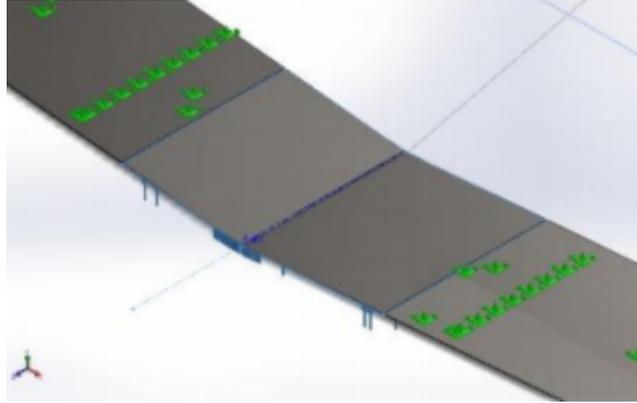


Figure 2: (Top) Side view of the matrix band. This represents the side view of both the prototype and the control as the cutout cannot be seen from this view. (Bottom) Top-side view of the final prototype. This view shows how the 62% incline was added. The thickness of the middle is 0.0038 cm, while the two lines that are 0.5cm away are 0.0061 cm.

Discussion

A static test was performed on both bands with the same fixtures and loads. A solid mesh was placed on the material and the portion of the band outside of the area changed to eliminate any movement from the sides of the band. This was important as the only area we were concerned about was the area receiving the forces. An elastic support was added to the sloped part of the prototype and one side of the control band in the 1 cm area near the middle, because in the clinic, the sloped side of the prototype would be in contact with the adjacent tooth, while the flat side would be in contact with the filling composite. This was used to reduce the allowed deformation to match the small amount that could occur between the teeth when separated. This distance was set at 0.00508 cm, which is the thickness of the larger of the two bands used in practice. To get this value, multiple tests were run to get to this deformation on the control band. This was found to be a 351.5 kg/in² stiffness value in SolidWorks. Finally, a force was placed on the opposite side of the elastic support in the 1 cm area around the middle. This force was set at 0.544 N to mimic the force a dentist would be putting on the matrix band when contouring the new filling. This was experimentally determined by pushing on a scale with similar force a

dentist would use. This force was found to be 0.272 N, but a factor of safety of two was added to account for error.

The control band resulted in a 90.46 MPa max stress, which was focused on the sides of the elastic support area. Figure 3 shows the distribution of the stress around where the force was applied. The orange area shows where the stress was highest. Since the yield stress of the AISI Type 316L stainless steel is 170 MPa, this design, unsurprisingly, does not fail. However, the proposed design had a 249 MPa max stress concentrated in the middle of the band. The section of the band with half thickness tore as the max stress in that area was greater than the yield stress. The testing parameters and results are outlined in more detail in the appendix.

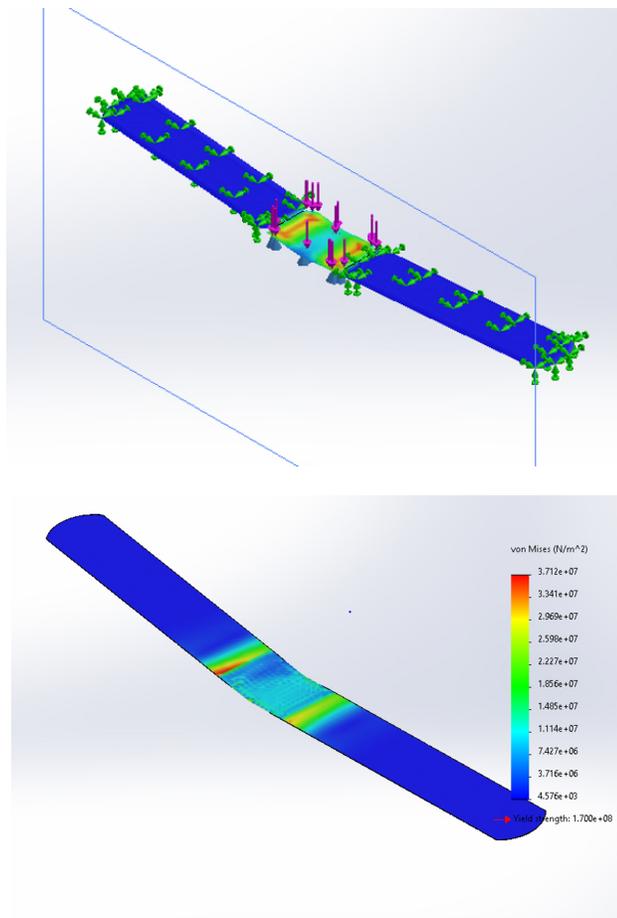


Figure 3: (Top) Stress distribution for the control band. The highest stresses are concentrated in the orange areas. (Bottom) Stress distribution for the final design. With an increased thickness, the band no longer failed.

Although this test showed that the design failed, there are multiple explanations for this. The factor of safety was set at two, but since the repercussions of breakage are not very

detrimental to the patient's health, a factor of safety of 1.5 might be sufficient. The force used was also not entirely accurate as the team decided on the force without having expertise in the field. In order to get a more accurate force value, a dentist should be the one using the scale. One other big factor that could be changed is the thickness of the middle of the band where the tear took place. Matrix bands used in dentistry today are either 0.00381 or 0.00508 cm thick. Since this experiment used a thickness of 0.00381 cm, there would still be 0.00127 cm of extra space that could be used. This could be incorporated by either decreasing the slope used to cut the band and ending at a larger thickness or by increasing the full thickness of the band, which would increase the thickness of the middle to 0.00254 cm instead of 0.002 cm. Both scenarios would increase the thickness of the 1 cm area, which would lead to a decrease in stress. If this decrease in stress is less than the yield stress, then this design could still be viable. For the final prototype that was outsourced, a 0.00254 cm middle thickness was used to decrease the stress put on the band. With these dimensions the band did not fail, as seen in figure 3. Next, physical mechanical testing was done to determine if the band would hold up to stresses put on it in the clinic.

To physically test the mechanical properties of the band, a MTS machine was used. When these tests were done, the final outsourced prototype had not arrived, so a traditional tofflemire band was used along with feeler gauges of 0.0015 in and 0.002 in thicknesses. Using these three different bands allowed the team to compare the results of a thicker band with a thinner band to see how drastic the difference would be. Since the band was so small compared to usual materials tested in the MTS machine, the machine was set to move at 10 mm/min for all tests. All three tests failed as the band slipped out of the clamp on either the top or bottom. Since the bands did not ever fail and most likely no strain was recorded, the plots developed from the stress-strain response are not accurate and should not be further studied. Figure 5 shows the bands after the test was completed and the area of slip can be seen at the end. The top of Figure 4 shows the stress-strain curves but they don't accurately represent the mechanical properties of the different bands.

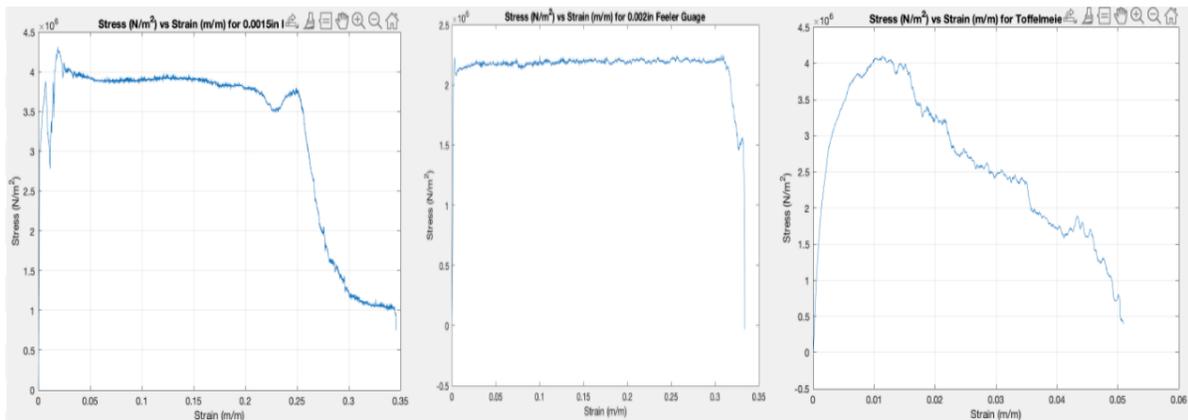


Figure 4: (left) Stress-strain curves for each trail. From left to right: 0.0015in feeler gage, 0.002in feeler gage, 0.0015in Tofflemire band.



Figure 5: 0.0015 in feeler gauge, 0.0015in tofflemire bands, and 0.002 in feeler gauge (top to bottom) post testing in MTS machine.

The team decided not to complete mechanical testing once we received the bands due to time constraints and not knowing how to test the bands properly. In the future, the bands should include a t-bone shape to allow for more grip in the MTS machine. Only the mechanical properties of the middle portion, which would be the same design as the final prototype, would be tested, but there would be more support. This should reduce all slip and allow for accurate results. Once results are obtained, they can then be compared against a regular Tofflemire band. Another test that would be useful would be to test the compressive strength of the band.

To assess the overall functionality of the band, we ranked the ease of use and practicality according to a battery of performance tests by which a team member engaged with the device and compared the double hug band's effectiveness and ease of use to the device currently in use: the tofflemire band. The tests compared and contrasted the tofflemire band with the double hug band, as our device is intended to be an improved iteration of the tofflemire. Prior to testing, we established that if the double hug band failed to outperform the tofflemire band, we would have to make design adjustments. The results of these tests gave us information to qualitatively and semi-quantitatively determine the overall functionality, structural integrity, and ease of use of the "doublehug" matrix band. A team member assessed several criteria detailed in the testing protocol (see Appendix) by ranking the device on a scale of 1-5 by the metrics outlined in the survey (detailed in Appendix). The team member was also prompted to make comments on any observations made that the survey did not entail. Furthermore, each question was assigned a point value (1-5), and the scores were tallied to quantitatively determine whether the double hug design was eligible to move forward in the prototyping process or undergo further refinement (according to the inadequacies noted in the assessment). The double hug scored 47/65, and this is considered a failing score according to our outlined standard (a score in the top 5% was deemed to ideal). Although the initial battery of tests indicated a failed design, we intend to redo this set of tests at least 4 more times with different people to get an average score that may give a better estimate of how functional the device is. As the functionality testing protocol is highly subjective, an average of scores from different perspectives will give us a better idea of the device's true physical character.

Conclusions

The viability of the matrix band design proposed is contingent on its functionality testing and mechanical testing success, and considering that the first functionality assessment executed resulted in a failed performance score, and given our inability to produce accurate mechanical testing results, we cannot definitively say whether our design proves to be a viable solution to the problem at hand. From the data collected this semester, we believe it would be wise to improve our testing methods and strategies in the following ways in order to obtain accurate data that gives us some insight on the performance of our device. First, we will need to find a method to

cut some of our matrix band prototypes into dog bones, so when testing in the MTS machine, we can avoid the slipping experienced while testing this semester. Secondly, as iterated before, we will also seek to have 5 randomly chosen people assess the functionality of the prototype according to the questionnaire provided, and with this compiled data, we can determine the mean functionality test score to more accurately depict the device's ease of use and physical character.

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Appendix

Product Design Specifications (PDS)

Function:

Matrix bands are a commonly used dental tool which assist dentists by providing a wall to maintain a tooth's structure and shape during restorative procedures, such as cavity fillings[1]. During typical filling procedures--particularly filling cavities on interproximal surfaces--dentists must fill one tooth at a time since matrix bands cannot be placed adjacent to one another, as the thickness of two bands exceeds the aperture diameter between the teeth. The resulting process of placing matrix bands for both teeth is cumbersome and time inefficient. The proposed design should alleviate the need to repeatedly place bands by employing a dual band system which is thin enough to securely and comfortably fit in between the affected teeth and able to simultaneously fit the appropriate convex/concave contour of each tooth. The finalized product should also maintain the tensile strength, malleability, and space efficiency of current matrix bands.

Client Requirements

1. Function Importance (as ranked by the client)
 - a. Device must be able to securely fit to the convex/concave contour of 2 adjacent teeth undergoing restoration
 - b. Device should be equivalent or less costly to manufacture as compared to existing matrix bands
 - c. Device must remain inert in the presence of filling materials (amalgam, ceramic, composite etc.)
 - d. Device should not be obstructive or clash with other tools to be used (rotary instruments, mirrors, forceps, suction etc.)
 - e. Device material must be non-toxic
 - f. Device should be thin and have high tensile strength

Design Requirements

1. Physical and Operational Characteristics

- a. *Performance requirement*
 - i. Must include some mechanism to maintain adequate separation between teeth being filled (the appropriate spacing is to be determined)
 - ii. The device must include some fence-like feature which is capable of fitting both concave and convex curvature of the adjacent teeth undergoing repair
 - iii. Device material must be malleable and able to easily bend to shape according to the tooth's contour
 - iv. Device material must be thin enough (dimensions to be determined) to be secured between the adjacent teeth, and it must have a high tensile/compressive strength(force to be determined) to withstand manipulation
- b. *Safety*
 - i. This device must adhere to safety standards/ regulations (if any) specified by the FDA as a class I device[2]
 - ii. Labelling should include instruction for proper installation and handling to avoid harm to the patient and ensure sterility
 - iii. Warnings should discourage use of the device if sterilized packaging has been tampered or if the device appears damaged
 - iv. Device should be handled with the appropriate tools (i.e. forceps, cotton pliers etc.[3])
- c. *Accuracy and Reliability:*
 - i. The band matrix should range in thicknesses of 0.0254 mm to 0.0508 mm (approximately the thicknesses of the commonly used universal Tofflemire Matrix Bands[4])
- d. *Life in Service:*

- i. The device must maintain its structural integrity and form throughout the duration of a standard filling procedure (approximately 1 hour [5])
 - ii. This device is intended for single use
- e. *Shelf Life:*
 - i. The device must should stable and sterilized, if left in its original sterilized packaging, for an indefinite amount of time
 - ii. If device packaging is compromised, it is no longer fit for use and should be disposed in the appropriate sharps collection container
 - iii. Must be stored in dry, temperate conditions.
- f. *Operating Conditions:*
 - i. The device should maintain structural integrity within the span of ambient and body temperature, from 20°C to 37°C.
 - ii. The device should be able to withstand high humidity and moisture levels for the span of time in which it is in use, in the patient's mouth.
- g. *Ergonomics*
 - i. The device should not be more difficult to use than the current retainer and band method, preferably a similar system.
- h. *Size*
 - i. The device must be thin enough to fit between two separate teeth in a patient's oral cavity
 - ii. The device must have variable matrix height to account for different teeth within the mouth, as well as different patients
 - iii. The device must be small enough to maintain maneuverability within the oral cavity, as to make the application of the band, and subsequently the filling, easier.

j. *Materials:* The current device is being made with stainless steel or aluminum. This material the bands would be made of would most likely be some form of strong metal to be a rigid wall and resist deformation.

k. *Aesthetics, Appearance, and Finish:* Aesthetics are not the biggest concern. It cannot be covered in any material that would be considered toxic due to insertion of this device in the mouth. The bands are typically made out of metal, and the device as a whole will be made of mostly metal and plastic of no particular aesthetic and appearance.

2. Production Characteristics

a. *Quantity*: This project requires only one unit of the device to be developed. In the end, many of these devices will need to be created at a low cost in order to be used commonly or commercially

b. *Target Product Cost*: The goal of this project is to keep the bands low cost similarly to the cost of other bands. Currently bands can be purchased at a fairly low cost, anywhere from .50 cents to one dollar per band. [6] The project's band would most likely have to be around this cost. Additionally, in this projects past the handle piece parts totaled around \$300, so this cost can be the target for the reusable handle piece.

3.

Miscellaneous

a. *Standards and Specifications*: This device will have direct contact with the patient, so FDA approval is required. In the Code of Regulations Title 21, Chapter 1, Subchapter H, and Part 872, the dental matrix band is mentioned as a Class I device. If the device designed is made with the same materials as previously FDA approved matrix bands before 1976, then the device would be exempt from premarket notification processes 510(k). However, if it was made with materials used in later devices, it would need to go through that process, which requires a 90 day notice to the FDA before marketing the product [7]. Other FDA documents and steps would be required including the establishment registration, listing the medical device to the FDA, obtaining an investigational device exemption if doing clinical studies, a quality system regulation, following labeling requirements, and reporting the medical device if necessary [8]

b. *Customer*: The two primary targets for this device would be dentists and dental supply companies. Therefore, maintaining standards and outcompeting competition is especially important. As the client is a dentist himself, the customer specifications are very similar to the client specifications in that the device should decrease procedure time, improve proximal contact, and correctly contour the tooth.

c. *Patient-related concerns*: As this device will come in contact with a patient's oral cavity, it is extremely important that the materials it is made of are non-toxic and provide no harm to the patient. The device should also not provide discomfort, as getting the filling in itself will already be uncomfortable. Since this will be a one-time use device, no sterilization of the band will be needed. The retainer, however, will need to be sterilized if it is used on another patient. The device should also not increase procedure time.

d. *Competition*: Although there are many similar devices on the market, they all don't allow for the filling of more than one tooth at a time. There are two devices that allow for this, which is called the Trident V3 Ring and the Trident Wave-Wedge, which are both used to separate adjacent teeth. While the device is in, matrix bands can be placed around both teeth. Although this method does work in theory, the contact is not optimal. By using two matrix bands between the teeth, the gap can be bigger than anticipated in both methods [9].



Figure 1: Using the Trident to spread the adjacent teeth to place two separate matrix strips. This allows for the filling of two adjacent teeth simultaneously [9].



Figure 2: Using the Wave-Wedge from Trident to separate the adjacent teeth during filling [9].

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8. U.S. Food and Drug Administration. 2020. *Overview Of Device Regulation*. [online] Available at: <<https://www.fda.gov/medical-devices/device-advice-comprehensive-regulatory-assistance/overview-device-regulation#ide>>
9. Jeffrey M. Rosenberg, D., 2020. *Making Contact: A Method For Restoring Adjacent Posterior Direct Resin | Dentistry Today*. [online] Dentistrytoday.com. Available at: <<https://www.dentistrytoday.com/restorative/8821-making-contact-a-method-for-restoring-adjacent-posterior-direct-resin>>

Preliminary Designs

- *Design 1: The Butterfly*

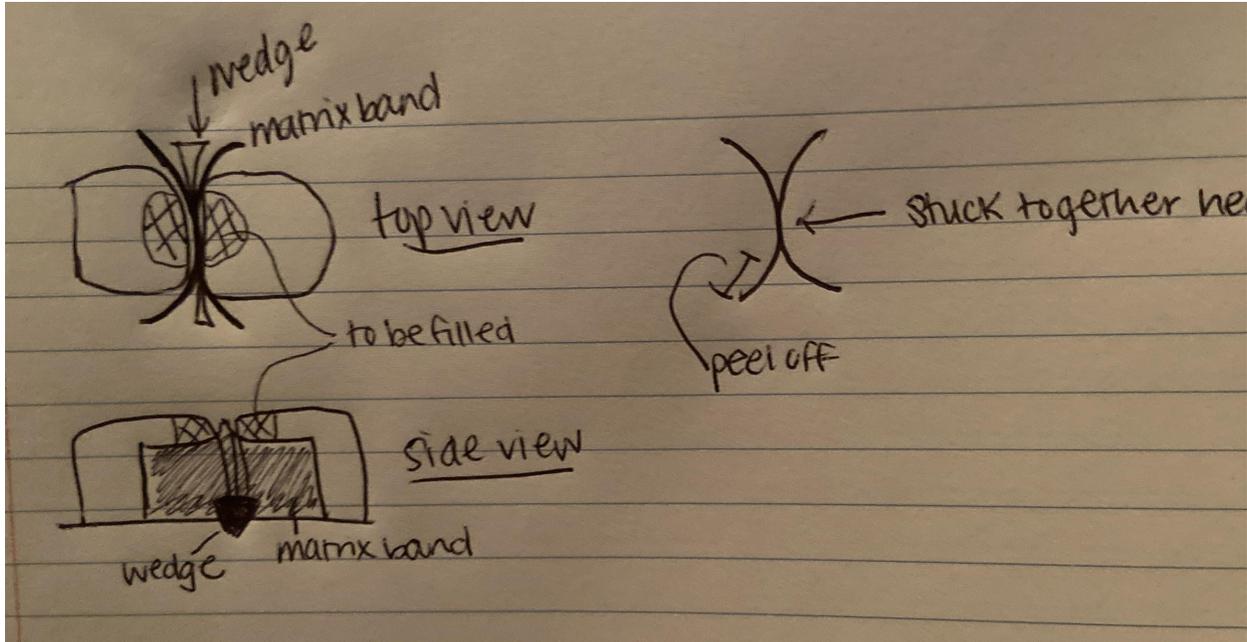


Figure 5: Sketch of the “butterfly” design. The crosshatched area is where the filling would need to be placed.

The butterfly consists of one matrix band that has two sections on either side of it that peel apart. These two sections can be contoured around the adjacent teeth on both sides making it possible to do two fillings at once. The peel feature also allows you to adjust the band size in order to accurately fit the patient’s teeth. The part of the band that stays between the teeth would be permanently stuck together to give more stability. This part would also only be the thickness of one band to give a better contact between the teeth after filling. There would also be a wedge inserted between the teeth to give more separation during the procedure, which allows for the spring back to happen once the wedge is removed, which also promotes close contact between the teeth. The two ends would be two bands thick, but once peeled apart they would be the thickness of bands used today, which would allow for increased stability around the adjacent teeth. With this design you could either use a retainer or a Palodent ring to hold the band in place.

- ***Design 2: The DoubleHug (Doug)***

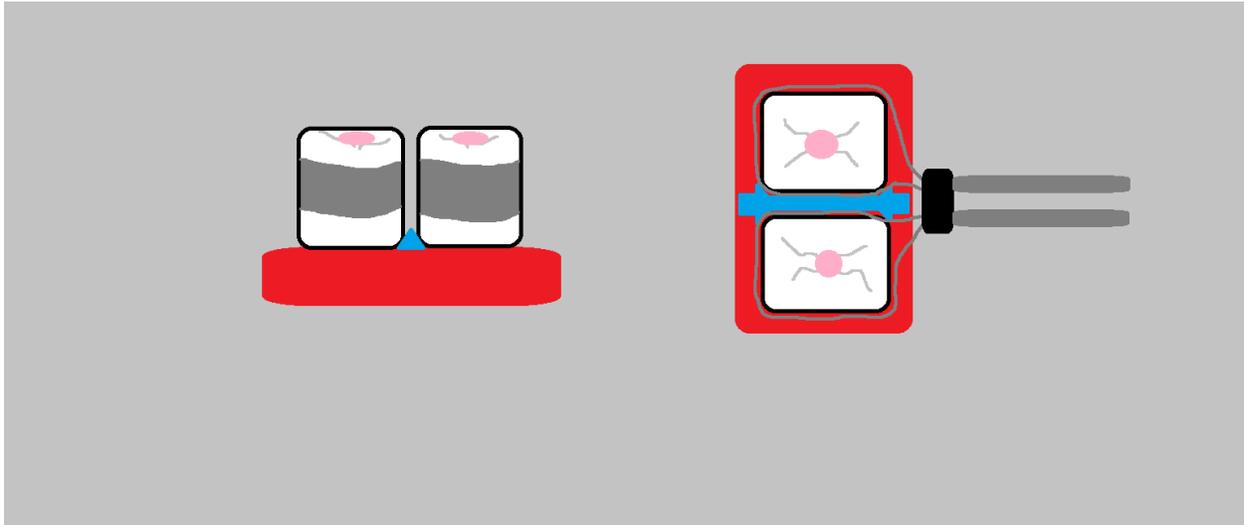


Figure 6: Model of the Doug design showing a top and side view. The blue portion is the wedge, the bands are in silver, and the teeth are white.

The Doug consists of a similar mechanism to the current model, but rather than one tightening system on one band, its two separate tightening mechanisms on two independent bands within the same device. This device is promising as it is simply making the current model function as two, without the ergonomic complications of two separate devices. The sole issue at hand with this model is that the width of two matrix bands during the filling process makes the junction between the teeth too weak once the fillings are complete, so we are researching methods, including material adjustments, to thin out the bands and allow for a tighter fit post-filling.

- ***Design 3: The Potato Wedge***

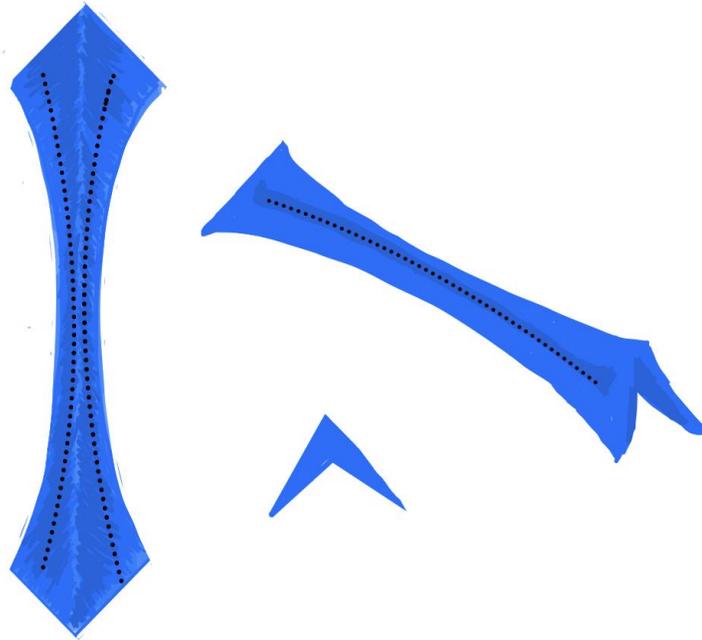


Figure 7: Sketch of the potato wedge design showing all views. The dotted lines are where the bands would be placed.

This design closely resembles the Insert Palodent® plus wedge guard, however, the Potato Wedge incorporates slit inserts on the sides where matrix bands may be inserted and shaped to the respective curvature of the adjacent teeth. The premise of this design is to incorporate a mechanism which ensures the secure placement of two bands for each tooth while maintaining the natural spacing. Ideally, the wedge may be easily slid into place between the two teeth undergoing restoration (as a typical wedge currently on the market would), and the bands can easily slide into place between the teeth. This design is also promising as sectional bands have shown to have better contact post filling over circumferential bands. [24]

Preliminary Design Evaluation

● *Design Matrix*

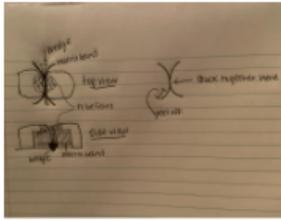
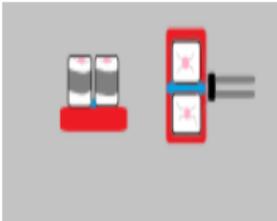
	The Butterfly! 🦋 	(Doug) DoubleHug 	The Potato Wedge 🥔 
Safety (30)	24 (4)	30 (5)	18 (3)
Effectiveness (20)	16 (4)	20 (5)	16 (4)
Cost (20)	16 (4)	20 (5)	12 (3)
Adjustability (15)	12 (4)	15 (5)	6 (2)
Patient Comfort (10)	8 (4)	6 (3)	10 (5)
Ergonomics (5)	5 (5)	4 (4)	5 (5)
Total	81	95	67

Table 1: The six design criteria on the far-most left column were evaluated for each preliminary design. Each design was given a number score out of 5 for each category. Finally, each design's ratings were totaled to determine which design was best. Dark green shaded blocks indicate the highest ranking in each category.

Safety

Safety was ranked as our highest category, as ensuring the wellbeing of the patient is of utmost priority and importance. This involves having bioinert, nontoxic materials in our design, as well as ensuring there are no cutting edges that could possibly harm the patient. The Doug design was ranked highest in this category due to the assurances given since this is a modification of the current design in use today.

Effectiveness

Effectiveness is ranked next on our list, as the function of the device is crucially important. If the device doesn't function at least as well as the current design in terms of both

quality and time, then the device is useless. This describes how well the teeth can be filled, as well as how close the teeth are to each other post-filling. The Doug design also ranked highest in this category, as it can function exactly the same as the current design in use, just twice as fast.

Cost

Cost is ranked equally with effectiveness, as if the design we are making isn't at least the same price as the model in use today, then there is no point in using it. The potato wedge was the lowest of the three, as it would require purchasing or modeling of a separate rubber material, something in which the other two designs do not require, and the butterfly requires some manipulation of matrix bands which would possibly eat through more cost.

Adjustability

Adjustability was ranked next, and this describes the ability for the device to be manipulated to function on different sized and shaped teeth, all while maintaining function. The Doug won this category as it allowed for both bands to be adjusted during use, whereas the potato wedge and butterfly would be much harder to adjust during, or slightly prior to insertion.

Patient comfort

This describes how unpleasant the operation would be for the patient, and the Potato Wedge won this category as it is the smallest design, keeping the patient from possibly gagging and having a terrible experience.

Ergonomics

This describes the ease-of-use for the dentist themselves, and all scored fairly well, but the Doug lost a point as the double articulation might be slightly cumbersome during the operation, while the other two have no arms reaching from the filling site.

10. Proposed Final Design: Doug

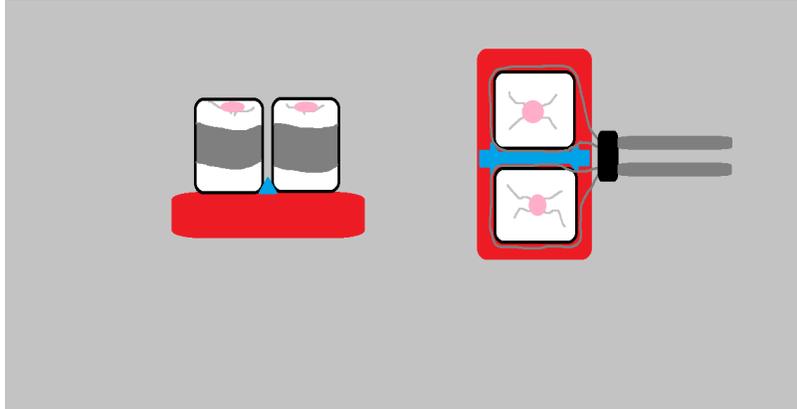


Figure 8: Repeated image of the Doug design.

The Team has decided to continue with the Doug design, as the assurance of functionality is a comfort, and the modifications that must be made to increase efficiency seem achievable. This design is the simplest design created, as it incorporates a lot of the current design aspects and only includes a thinner band and bigger retainer.

Testing Protocols

● **Functionality Testing Protocol**

** insert images of procedure once we have prototype

**clarify the demarcation of the thinner portion of the band

Premise: These tests will be used as an assessment to qualitatively determine the overall functionality, structural integrity, and ease of use of the “doublehug” matrix band.

Materials:

1. Doublehug matrix band prototype
2. Universal tofflemire matrix band (0.0015 thickness)
3. 2, standard universal matrix band retainers
4. Palodent wedge guard--tooth wedge
5. Standard adult teeth model

Procedure:

1. Place the palodent wedge guard in between the molars undergoing mock restoration

2. Take one of the double hug bands and bend it to the appropriate shape of one molar making sure the area of the band marked with a rectangle (the portion with the thinner cross section area) is placed in between the tooth contact gap
 - a. Make note on the provided questionnaire how strenuous is it to bend the band to shape (1-much effort and force is required, 5- very little effort and force is required)
 - b. Make note on the provided questionnaire how much force is required to fit the band between the contact gap (1- much force is required to fit the band between the teeth--very tight fit, 5- very little force is required to fit the band between the teeth--seemingly appropriate fit)
3. Tighten the 1st band using the retainer (as typically performed in a clinical setting)
4. Take the second double hug band and, again, bend it to the appropriate shape of the adjacent molar making sure the area of the band marked with a rectangle is placed in between the teeth
 - a. Make note on the provided questionnaire how strenuous is it to bend the band to shape (1-much effort and force is required, 5- very little effort and force is required)
 - b. Make note on the provided questionnaire how much force is required to fit the band in between the contact gap (1- much force is required to fit the band between the teeth--very tight fit, 5- very little force is required to fit the band between the teeth--seemingly appropriate fit)
 - c. Make note on the provided questionnaire if there is a distortion of the band shape once both bands are placed next to each other (1- there is severe bending/distortion of the curvature of one/both bands upon inserting the second band, 5- there is no bending/distortion of the curvature of one/both bands upon inserting the second band)
5. Tighten the 2nd band using another retainer (as typically performed in a clinical setting)
6. On the questionnaire, provide any other comments pertaining to the rigidity of the interproximal part of the band (1- the band is relatively flimsy and the contour is easily disrupted by placing light force against it, 5- the band is appropriately rigid and the contour is not disrupted by placing light force against it)
7. Under each question on the questionnaire, elaborate on any observations that are not adequately communicated by ranking from 1-5.
8. On the molars on the opposite side of the mouth, perform a standard set up for a mock restoration

****Steps 9-15 are simply steps 1-7 performed again but using a tofflemire band. The point of the following is to gauge the performance similarities/ discrepancies between the two bands. All the ranks assigned should be the toffelmier performance AS COMPARED TO the double hug band (1 indicates underperformance of the toffelmier compared to double hug, 3 indicates no significant difference between the two, 5 indicated overperformance of toeffelmeier compared to double hug)**

9. Place the palodent wedge guard in between the molars undergoing mock restoration

10. Take one of the tofflemire bands and bend it to the appropriate shape of one molar. Make note on the provided questionnaire how strenuous is it to bend the band to shape (1-much effort and force is required, 5- very little effort and force is required)
 - a. Make note on the provided questionnaire, **as compared to the double hug band**, how strenuous is it to bend the band to shape (1-much effort and force is required compared to the double hug band, 5- very little effort and force is required compared to the double hug band)
 - b. Make note on the provided questionnaire, **as compared to the double hug band**, how much force is required to fit the band between the contact gap (1- much force is required to fit the band between the teeth--very tight fit compared to the double hug band, 5- very little force is required to fit the band between the teeth--seemingly appropriate fit compared to the double hug band)
11. Tighten the 1st band using the retainer (as typically performed in a clinical setting)
 - a. Make a written note of any differences experienced in tightening the toffelmier band vs double hug band (i.e. differences in resistance, security etc.)
12. Take the second toffelmier band and, again, bend it to the appropriate shape of the adjacent molar
 - a. Make note on the provided questionnaire, **as compared to the double hug band**, how strenuous is it to bend the band to shape (1-much effort and force is required compared to the double hug band, 5- very little effort and force is required compared to the double hug band)
 - b. Make note on the provided questionnaire, **as compared to the double hug band**, how much force is required to fit the band between the contact gap (1- much force is required to fit the band between the teeth--very tight fit compared to the double hug, 5- very little force is required to fit the band between the teeth--seemingly appropriate fit compared to the double hug)
 - c. Make note on the provided questionnaire, **as compared to the double hug band**, if there is a distortion of the band shape once both bands are placed next to each other (1- there is severe bending/distortion of the curvature of one/both bands upon inserting the second band compared to the double hug, 5- there is no bending/distortion of the curvature of one/both bands upon inserting the second band compared to the double hug)
13. Tighten the 2nd band using another retainer (as typically performed in a clinical setting)
14. On the questionnaire, provide any other comments pertaining to the rigidity of the interproximal part of the band, **as compared to the double hug band**, (1- the band is relatively flimsy and the contour is easily disrupted by placing light force against it compared to the double hug, 5- the band is appropriately rigid and the contour is not disrupted by placing light force against it compared to the double hug)
15. Again, under each question on the questionnaire, elaborate on any observations that are not adequately communicated by ranking from 1-5.

● Qualitative Doug (Double Hug) Functionality Performance Assessment

Doug Double Hug Band One

1. How strenuous is it to bend the band to shape?(1-much effort and force is required, 5-very little effort and force is required). Circle one.

1 2 3 4 5

2. How much force is required to fit the band in between the contact gap (1- much force is required to fit the band between the teeth--very tight fit, 5- very little force is required to fit the band between the teeth--seemingly appropriate fit). Circle one.

1 2 3 4 5

3. Assess the rigidity of the interproximal part of the band (1- the band is relatively flimsy and the contour is easily disrupted by placing light force against it, 5- the band is appropriately rigid and the contour is not disrupted by placing light force against it)

1 2 3 4 5

*Additional Comments:

Doug Double Hug Band Two

1. How strenuous is it to bend the band to shape?(1-much effort and force is required, 5-very little effort and force is required). Circle one.

1 2 3 4 5

2. How much force is required to fit the band in between the contact gap ? (1- much force is required to fit the band between the teeth--very tight fit, 5- very little force is required to fit the band between the teeth--seemingly appropriate fit). Circle one.

1 2 3 4 5

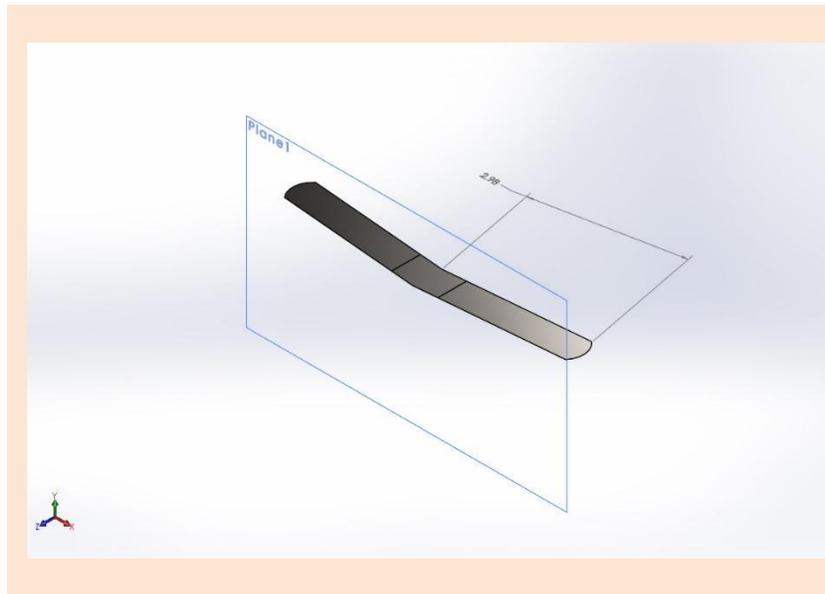
3. Is there a distortion of the band shape once both bands are placed next to each other ? (1- there is severe bending/distortion of the curvature of one/both bands upon inserting

*Additional Comments:

Total Score: / 65

Results

- ***Control Mechanical Testing Results***



Simulation of Control Matrix Band

Date: Wednesday, December 2, 2020

Designer: Solidworks

Study name: Static 2

Analysis type: Static

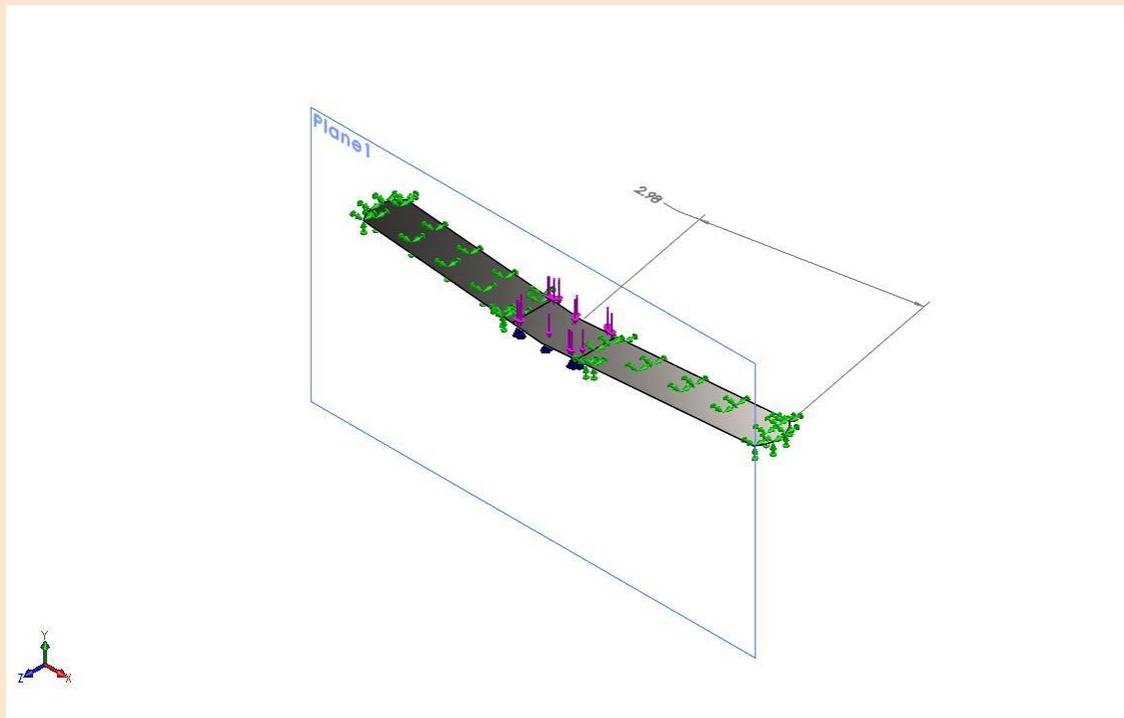
Description
Matrix band

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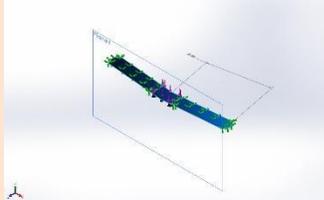
Assumptions

Model Information



Model name: matrixband NO CUT11-29-20solved
Current Configuration: Default

Solid Bodies

Document Name and Reference	Treated As	Volumetric Properties	Document Path/Date Modified
Split Line6 	Solid Body	Mass:0.000118152 kg Volume:1.47193e-08 m ³ Density:8,027 kg/m ³ Weight:0.00115789 N	\\Client\D\$\matrixband NO CUT11-29-20solved.SLDP RT Nov 29 11:44:24 2020

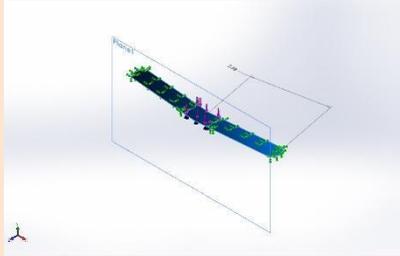
Study Properties

Study name	Static 2
Analysis type	Static
Mesh type	Solid Mesh
Thermal Effect:	On
Thermal option	Include temperature loads
Zero strain temperature	77 Fahrenheit
Include fluid pressure effects from SOLIDWORKS Flow Simulation	Off
Solver type	FFEPlus
Inplane Effect:	Off
Soft Spring:	Off
Inertial Relief:	Off
Incompatible bonding options	Automatic
Large displacement	Off
Compute free body forces	On
Friction	Off
Use Adaptive Method:	Off
Result folder	SOLIDWORKS document (\\Client\D\$)

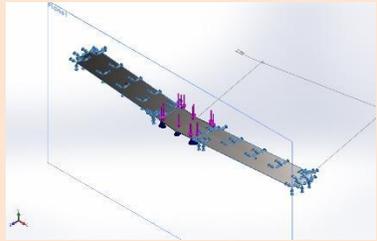
Units

Unit system:	SI (MKS)
Length/Displacement	mm
Temperature	Kelvin
Angular velocity	Rad/sec
Pressure/Stress	N/m ²

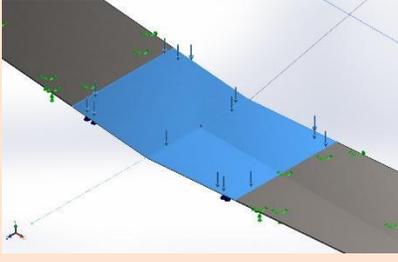
Material Properties

Model Reference	Properties	Components
	<p>Name: AISI Type 316L stainless steel</p> <p>Model type: Linear Elastic Isotropic</p> <p>Default failure criterion: Unknown</p> <p>Yield strength: 1.7e+08 N/m²</p> <p>Tensile strength: 4.85e+08 N/m²</p> <p>Elastic modulus: 2e+11 N/m²</p> <p>Poisson's ratio: 0.265</p> <p>Mass density: 8,027 kg/m³</p> <p>Shear modulus: 8.2e+10 N/m²</p> <p>Thermal expansion coefficient: 1.7e-05 /Kelvin</p>	SolidBody 1(Split Line6)(matrixband NO CUT11-29-20solved)
Curve Data:N/A		

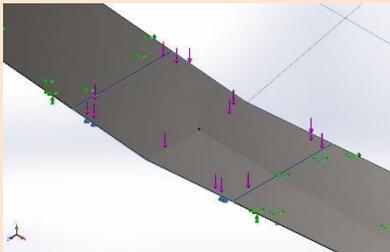
Loads and Fixtures

Fixture name	Fixture Image	Fixture Details		
Fixed-1		<p>Entities: 2 face(s)</p> <p>Type: Fixed Geometry</p>		
Resultant Forces				
Components	X	Y	Z	Resultant
Reaction force(N)	-0.0139348	0.905536	0.00270818	0.905648
Reaction Moment(N.m)	0	0	0	0

Load name	Load Image	Load Details
-----------	------------	--------------

Force-1		Entities: 1 face(s) Type: Apply normal force Value: 1.2 lbf
---------	---	--

Connector Definitions

Connector Name	Connector Details	Connector Image
Elastic Support-1	Entities: 1 face(s) Type: Elastic Support Normal stiffness value: 5,000 Shear stiffness value: 5,000 Units: (lbf/in)/in ²	 Elastic Support-1

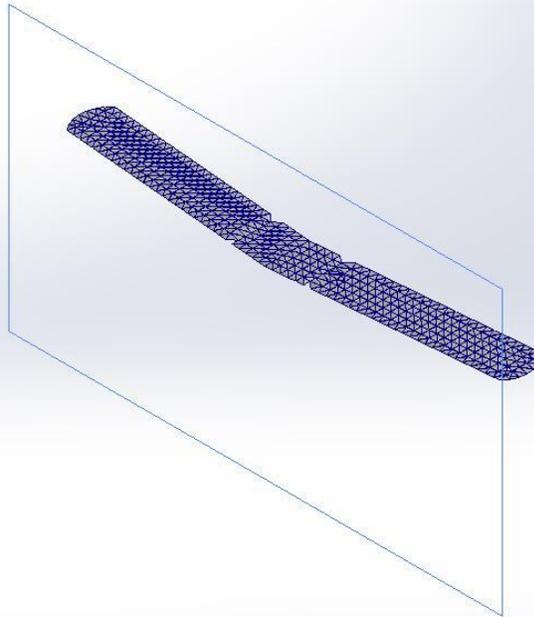
Mesh information

Mesh type	Solid Mesh
Mesher Used:	Standard mesh
Automatic Transition:	Off
Include Mesh Auto Loops:	Off
Jacobian points for High quality mesh	16 Points
Element Size	0.101795 cm
Tolerance	0.00508977 cm
Mesh Quality	High

Mesh information - Details

Total Nodes	4133
Total Elements	1874
Maximum Aspect Ratio	188
% of elements with Aspect Ratio < 3	0
Percentage of elements with Aspect Ratio > 10	100
Percentage of distorted elements	0
Time to complete mesh(hh:mm:ss):	00:00:03
Computer name:	WIN-3021

Model name: matrixband NO CUT11-29-20solved
Study name: Static 2(-Default-)
Mesh type: Solid Mesh



SOLIDWORKS Educational Product. For Instructional Use Only.

Sensor Details

No Data

Resultant Forces

Reaction forces

Selection set	Units	Sum X	Sum Y	Sum Z	Resultant
Entire Model	N	-0.00225955	5.3529	-0.00305129	5.3529

Reaction Moments

Selection set	Units	Sum X	Sum Y	Sum Z	Resultant
Entire Model	N.m	0	0	0	0

Free body forces

Selection set	Units	Sum X	Sum Y	Sum Z	Resultant
Entire Model	N	0.00964612	0.00910821	0.00145974	0.0133468

Free body moments

Selection set	Units	Sum X	Sum Y	Sum Z	Resultant
Entire Model	N.m	0	0	0	1e-33

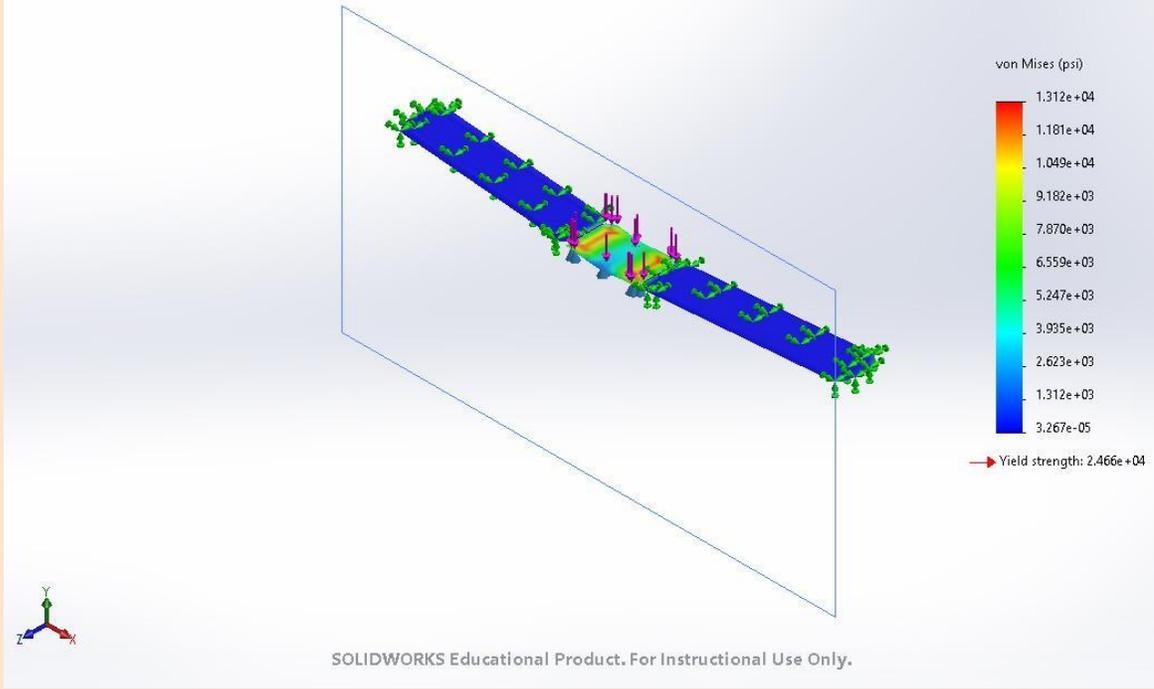
Beams

No Data

Study Results

Name	Type	Min	Max
Stress1	VON: von Mises Stress	0.225 N/mm ² Node: 3914	9.046e+07 N/mm ² Node: 404

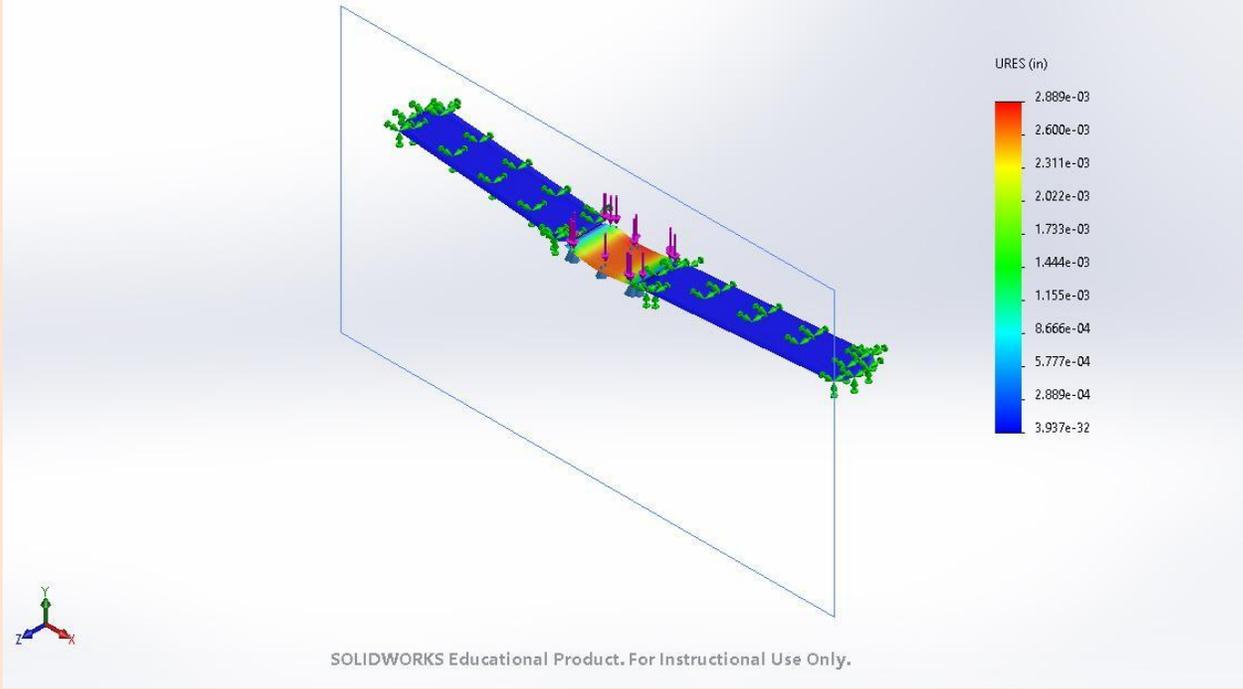
Model name: matrixband NO CUT11-29-20solved
 Study name: Static 2(-Default-)
 Plot type: Static nodal stress Stress1
 Deformation scale: 1



matrixband NO CUT11-29-20solved-Static 2-Stress-Stress1

Name	Type	Min	Max
Displacement1	URES: Resultant Displacement	0.000e+00in Node: 1	2.889e-03in Node: 199

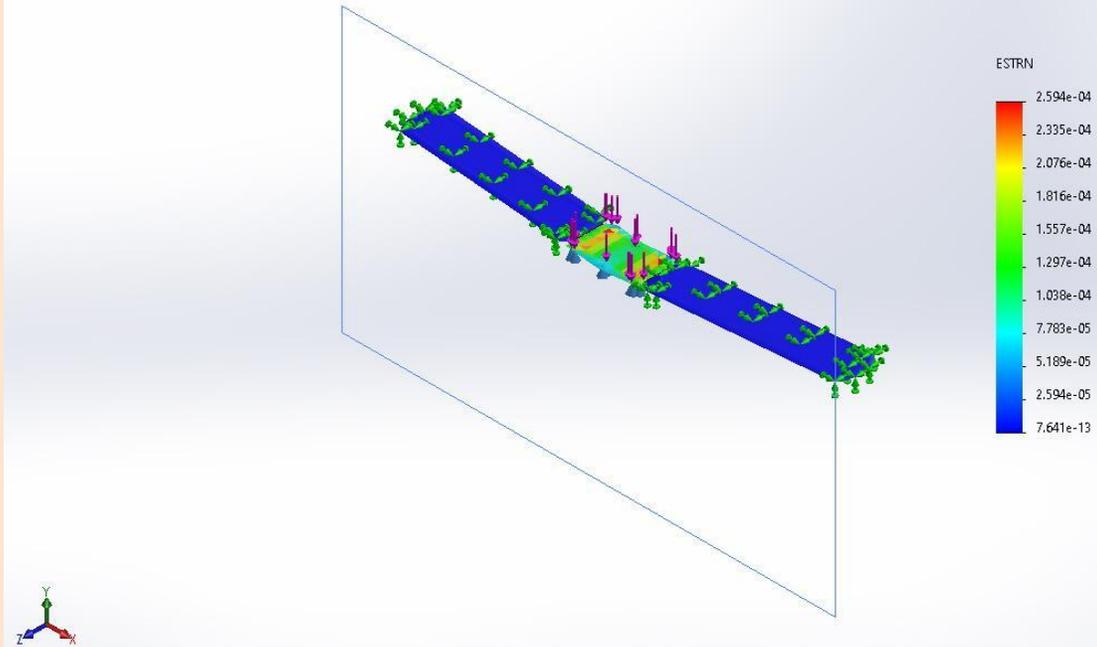
Model name: matrixband NO CUT11-29-20solved
 Study name: Static 2(-Default-)
 Plot type: Static displacement Displacement1
 Deformation scale: 5



matrixband NO CUT11-29-20solved-Static 2-Displacement-Displacement 1

Name	Type	Min	Max
Strain1	ESTRN: Equivalent Strain	7.641e-13 Element: 214	2.594e-04 Element: 1726

Model name: matrixband NO CUT11-29-20solved
Study name: Static 2(-Default-)
Plot type: Static strain Strain1
Deformation scale: 1



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matrixband NO CUT11-29-20solved-Static 2-Strain-Strain1

Simulation of Final Design

Date: Sunday, November 29, 2020
Designer: Solidworks
Study name: Static refined mesh-force
Analysis type: Static

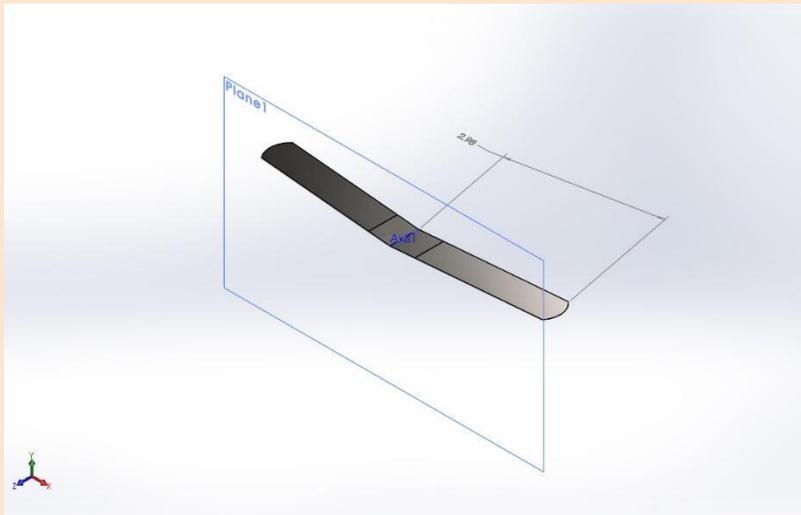


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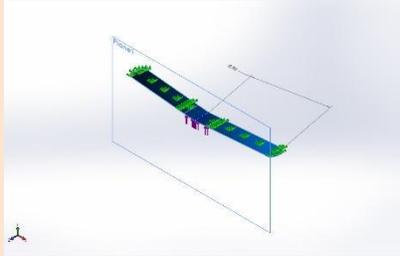
Study Properties

Study name	Static refined mesh-force
Analysis type	Static
Mesh type	Solid Mesh
Thermal Effect:	On
Thermal option	Include temperature loads
Zero strain temperature	298 Kelvin
Include fluid pressure effects from SOLIDWORKS Flow Simulation	Off
Solver type	FFEPlus
Inplane Effect:	Off
Soft Spring:	Off
Inertial Relief:	Off
Incompatible bonding options	Automatic
Large displacement	On
Compute free body forces	On
Friction	Off
Use Adaptive Method:	Off
Result folder	SOLIDWORKS document (I:\matrixband new11-28-20-Static 2)

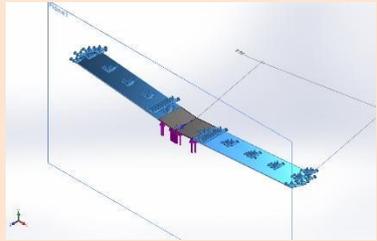
Units

Unit system:	SI (MKS)
Length/Displacement	mm
Temperature	Kelvin
Angular velocity	Rad/sec
Pressure/Stress	N/m ²

Material Properties

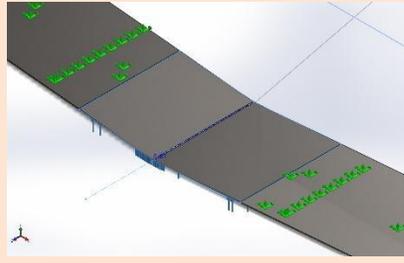
Model Reference	Properties	Components
	<p>Name: AISI Type 316L stainless steel</p> <p>Model type: Linear Elastic Isotropic</p> <p>Default failure criterion: Max von Mises Stress</p> <p>Yield strength: 1.7e+08 N/m²</p> <p>Tensile strength: 4.85e+08 N/m²</p> <p>Elastic modulus: 2e+11 N/m²</p> <p>Poisson's ratio: 0.265</p> <p>Mass density: 8,027 kg/m³</p> <p>Shear modulus: 8.2e+10 N/m²</p> <p>Thermal expansion coefficient: 1.65e-05 /Kelvin</p>	<p>SolidBody 1(Split Line1)(matrixband new11-28-20solvedfail)</p>
Curve Data:N/A		

Loads and Fixtures

Fixture name	Fixture Image	Fixture Details		
Fixed-1		<p>Entities: 2 face(s)</p> <p>Type: Fixed Geometry</p>		
Resultant Forces				
Components	X	Y	Z	Resultant
Reaction force(N)	-0.0124315	-0.858296	-0.000198672	0.858386
Reaction Moment(N.m)	0	0	0	0

Load name	Load Image	Load Details
-----------	------------	--------------

Force-1



Entities:
Type:
Value:

1 face(s)
Apply normal force
1.2 lbf

Contact Information

No Data

Resultant Forces

Reaction forces

Selection set	Units	Sum X	Sum Y	Sum Z	Resultant
Entire Model	N	-0.0223731	-5.21491	-0.0014857	5.21496

Reaction Moments

Selection set	Units	Sum X	Sum Y	Sum Z	Resultant
Entire Model	N.m	0	0	0	0

Free body forces

Selection set	Units	Sum X	Sum Y	Sum Z	Resultant
Entire Model	N	0	0	0	0

Free body moments

Selection set	Units	Sum X	Sum Y	Sum Z	Resultant
Entire Model	N.m	0	0	0	0

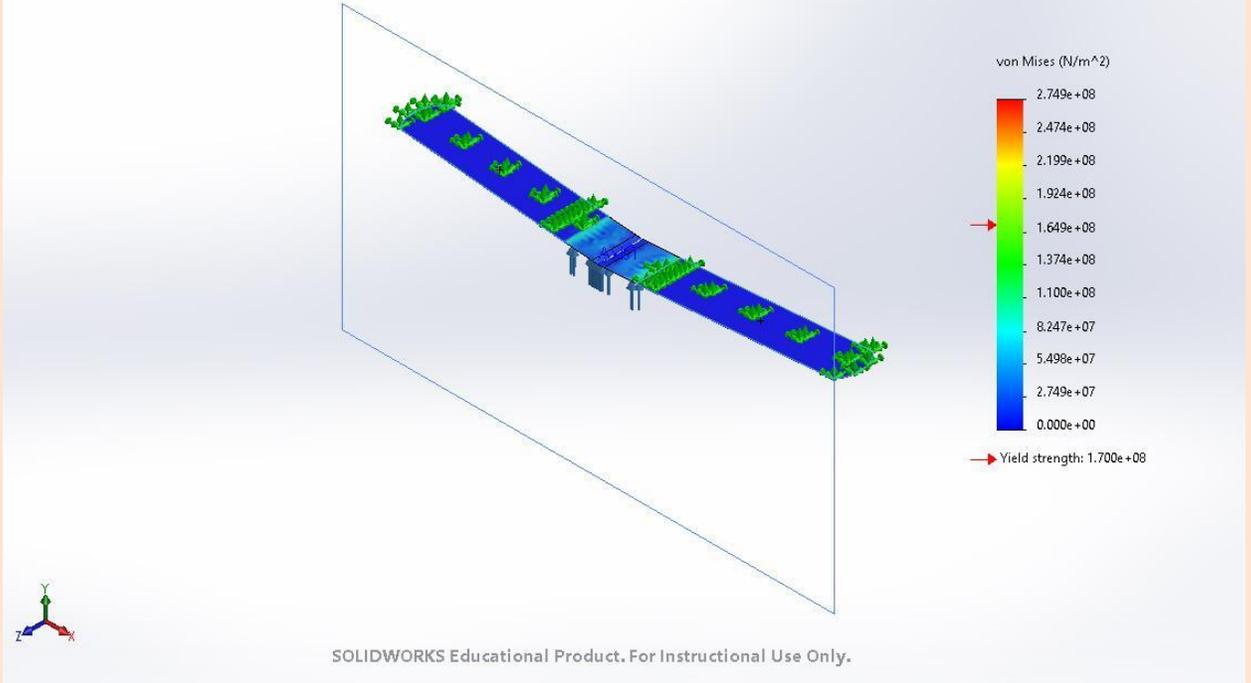
Study Results

Name	Type	Min	Max
Stress1	VON: von Mises Stress	0.000e+00N/m ²	2.749e+08N/m ²

Node: 21

Node: 4915

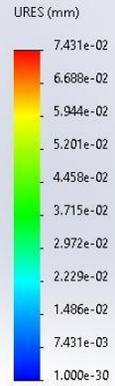
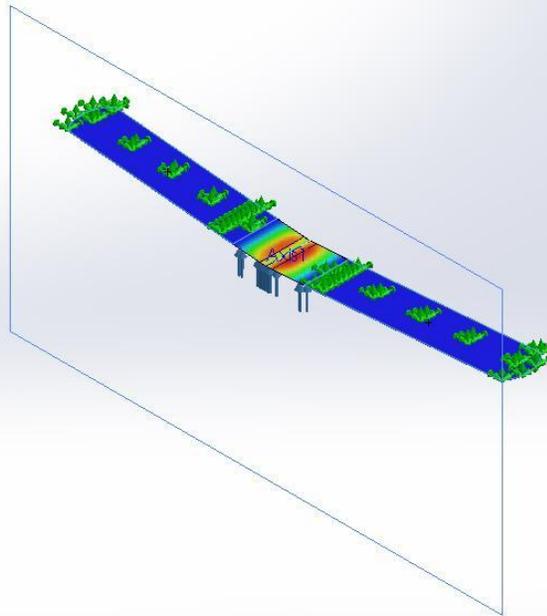
Model name: matrixband new11-28-20solvedfail
Study name: Static refined mesh-force(-Default-)
Plot type: Static nodal stress Stress1
Deformation scale: 1



matrixband new11-28-20solvedfail-Static refined mesh-force-Stress-Stress1

Name	Type	Min	Max
Displacement1	URES: Resultant Displacement	0.000e+00mm Node: 8	7.431e-02mm Node: 4803

Model name: matrixband new11-28-20solvedfail
 Study name: Static refined mesh-force(-Default-)
 Plot type: Static displacement Displacement1
 Deformation scale: 1

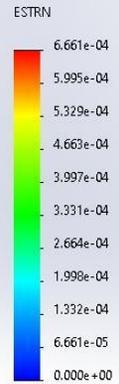
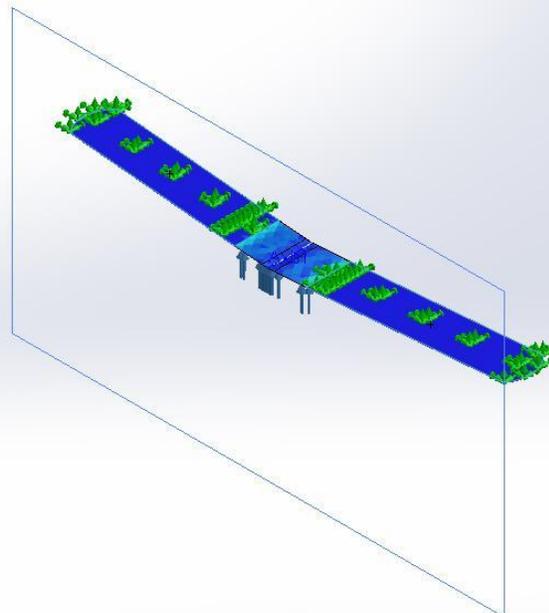


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matrixband new11-28-20solvedfail-Static refined mesh-force-Displacement-Displacement1

Name	Type	Min	Max
Strain1	ESTRN: Equivalent Strain	0.000e+00 Element: 1	6.661e-04 Element: 1856

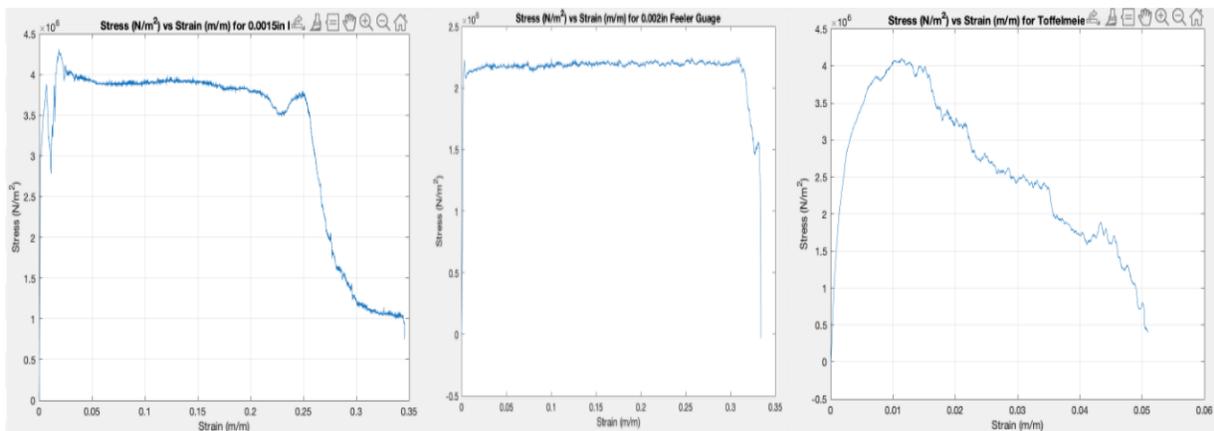
Model name: matrixband new11-28-20solvedfail
Study name: Static refined mesh-force(-Default-)
Plot type: Static strain Strain1
Deformation scale: 1



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matrixband new11-28-20solvedfail-Static refined mesh-force-Strain-Strain1

● Mechanical Testing (MTS) Results



- **Qualitative Doug (Double Hug) Functionality Performance Assessment : Assessment by Leah Gause**

Doug Double Hug Band One

1. How strenuous is it to bend the band to shape?(1-much effort and force is required, 5-very little effort and force is required). Circle one.

1 2 3 4 5

2. How much force is required to fit the band in between the contact gap (1- much force is required to fit the band between the teeth--very tight fit, 5- very little force is required to fit the band between the teeth--seemingly appropriate fit). Circle one.

1 2 3 4 5

3. Assess the rigidity of the interproximal part of the band (1- the band is relatively flimsy and the contour is easily disrupted by placing light force against it, 5- the band is appropriately rigid and the contour is not disrupted by placing light force against it)

1 2 3 4 5

*Additional Comments:

- The band is much easier to mold to the tooth

Doug Double Hug Band Two

1. How strenuous is it to bend the band to shape?(1-much effort and force is required, 5-very little effort and force is required). Circle one.

1 2 3 4 **5**

2. How much force is required to fit the band in between the contact gap ? (1- much force is required to fit the band between the teeth--very tight fit, 5- very little force is required to fit the band between the teeth--seemingly appropriate fit). Circle one.

1 2 3 **4** 5

3. Is there a distortion of the band shape once both bands are placed next to each other ? (1- there is severe bending/distortion of the curvature of one/both bands upon inserting the second band, 5- there is no bending/distortion of the curvature of one/both bands upon inserting the second band). Circle one.

1 2 **3** 4 5

4. Assess the rigidity of the interproximal part of the band (1- the band is relatively flimsy and the contour is easily disrupted by placing light force against it, 5- the band is appropriately rigid and the contour is not disrupted by placing light force against it). Circle one.

1 2 3 4 **5**

*Additional Comments:

- The bands effortlessly fit between the teeth

Tofflemire Band One

1. **As compared to the double hug band**, how strenuous is it to bend the band to shape? (1-much effort and force is required compared to the double hug band, 5- very little effort and force is required compared to the double hug band). Circle one.

1 2 3 4 5

2. **As compared to the double hug band**, how comfortably the band sits in between the contact gap (1- much force is required to fit the band between the teeth--very tight fit compared to the double hug band, 5- very little force is required to fit the band between the teeth--seemingly appropriate fit compared to the double hug band). Circle one.

1 2 3 4 5

3. Comment. Are there any differences experienced in tightening the toffelmier band vs double hug band (i.e. differences in resistance, security etc.)

Its harder to form a contour using the toffelmier band as compared to the double hug

*Additional Comments:

Tofflemire Band Two

1. **As compared to the double hug band**, how strenuous is it to bend the band to shape (1-much effort and force is required compared to the double hug band, 5- very little effort and force is required compared to the double hug band).Circle one.

1 **2** 3 4 5

2. **As compared to the double hug band**, how much force is required to fit the band in between the contact gap (1- much force is required to fit the band between the teeth--very tight fit compared to the double hug, 5- very little force is required to fit the band between the teeth--seemingly appropriate fit compared to the double hug). Circle one.

1 2 **3** 4 5

3. **As compared to the double hug band**, if there is a distortion of the band shape once both bands are placed next to each other? (1- there is severe bending/distortion of the curvature of one/both bands upon inserting the second band compared to the double hug, 5- there is no bending/distortion of the curvature of one/both bands upon inserting the second band compared to the double hug). Circle one.

1 2 **3** 4 5

4. Assess the rigidity of the interproximal part of the band, **as compared to the double hug band**, (1- the band is relatively flimsy and the contour is easily disrupted by placing light force against it compared to the double hug, 5- the band is appropriately rigid and the contour is not disrupted by placing light force against it compared to the double hug). Circle one.

1 2 3 4 **5**

*Additional Comments:

Total Score: 47 / 65

● MATLAB MS Testing Analysis Code

```
% Close figures and clear out other variables that have been assigned
close all;
clear all;
%%
%Test Run
% Load your data file
file_A = 'testrun8.txt';
data_A=load(file_A);

% Extract the columns of interest from your data
disp_A=data_A(:,1); force_A=data_A(:,2); time_A=data_A(:,3);

% Calculate test8 stress and strain
stress_A= force_A./ (0.013 * 0.0015);
strain_A= (disp_A./ 1000) ./ .0508;

%Plot test8 stress and strain (m)
figure(1);
plot(strain_A, stress_A);
xlabel('Strain (m/m)');
ylabel('Stress (N/m^2)');
title('Stress (N/m^2) vs Strain (m/m) for 0.0015in Feeler Gauge');
grid
%%
% Load your data file
file_B = 'testrun9.txt';
data_B=load(file_B);

% Extract the columns of interest from your data
disp_B=data_B(:,1); force_B=data_B(:,2); time_B=data_B(:,3);

% Calculate test8 stress and strain
stress_B= force_B./ (0.013 * 0.002);
strain_B= (disp_B./ 1000) ./ .0508;

%Plot test9 stress and strain (m)
figure(2);
plot(strain_B, stress_B);
xlabel('Strain (m/m)');
ylabel('Stress (N/m^2)');
title('Stress (N/m^2) vs Strain (m/m) for 0.002in Feeler Gauge');
grid
%%
% Load your data file
file_C = 'testrun10.txt';
data_C=load(file_C);

% Extract the columns of interest from your data
disp_C=data_C(:,1); force_C=data_C(:,2); time_C=data_C(:,3);

% Calculate test10 stress and strain
stress_C= force_C./ (0.006 * 0.0015);
strain_C= (disp_C./ 1000) ./ .0508;

%Plot test10 stress and strain (m)
```

```
figure(3);
plot(strain_C, stress_C);
xlabel('Strain (m/m)');
ylabel('Stress (N/m^2)');
title('Stress (N/m^2) vs Strain (m/m) for Toffelmeier Matrix Band');
grid
%%
% Load your data file
file_D = 'testrun11.txt';
data_D=load(file_D);

% Extract the columns of interest from your data
disp_D=data_D(:,1); force_D=data_D(:,2); time_D=data_D(:,3);

% Calculate test11 stress and strain
stress_D= force_D./ (0.006 * 0.0015);
strain_D= (disp_D./ 1000) ./ .0508;

%Plot test11 stress and strain (m)
figure(4);
plot(strain_D, stress_D);
xlabel('Strain (m/m)');
ylabel('Stress (N/m^2)');
title('Stress (N/m^2) vs Strain (m/m) for Toffelmeier Matrix Band');
grid
```